## AND8106/D

# 100 Watt, Universal Input, PFC Converter 

ON Semiconductor

## General Description

This 100 watt converter demonstrates the wide range of features found on the NCP1650. This chip is capable of controlling PFC converters well into the kilowatt range

In addition to excellent power factor, this chip offers fixed frequency operation in continuous and discontinuous modes of operation. It has a wide variety of protection features, including instantaneous current limiting, average current limiting, and true power limiting.

This unit will provide 400 V of well regulated power from an input source with a frequency range from 50 Hz to 60 Hz , and a voltage range of $85 \mathrm{~V}_{\mathrm{rms}}$ to $265 \mathrm{~V}_{\mathrm{rms}}$. It is fully self contained and includes a high voltage start-up circuit, and bias supply that operates off of the boost inductor.

## Features

- Fixed Frequency Operation
- Shutdown Circuit
- Operation Over the Universal Input Range
- Multiple Protection Schemes
- True Power Limiting
- Start-Up and Bias Circuits Included


## Circuit Description

## Start-Up Circuit

The start-up circuit allows the unit to use power from the input line to begin operation, and then shuts down to allow operation off of the bias winding, which reduces losses in the circuit.

The start-up circuit has three modes of operation. One is used for starting the NCP1650 when the chip is functional, one is for bias power during shutdown operation, and the third is the off state.

When power is initially applied to the unit, the gate of the pass transistor will be high, and the FET will be fully enhanced. The current into the $\mathrm{V}_{\mathrm{CC}}$ capacitance at pin 1 will be limited by the three $10 \mathrm{k} \Omega$ resistors in series with the FET.


Figure 1. Start-Up Circuit Schematic
This circuit will provide current as long as the FET is enhanced. For this to occur, the gate to source voltage must be greater than the gate threshold voltage. For this device that value is nominally, 4.0 V . The zener breakdown voltage is 18 V , so the FET will turn off at:

$$
\text { Vchg } \max =18 \mathrm{~V}-4.0 \mathrm{~V}=14 \text { Volts }
$$

As the output capacitor is charged up during the turn-on sequence, the bias supply voltage will also increase until the source of the FET exceeds 14 V . At this point, the FET will cease conduction, and all of the $\mathrm{V}_{\mathrm{CC}}$ power will be supplied via the bias circuit from the power inductor.
If the unit is commanded into the shutdown mode, the chip will reduce its bias current to 0.5 mA and the start-up circuit will then maintain a regulated voltage of approximately 14 V on the $\mathrm{V}_{\mathrm{CC}}$ pin until the device becomes operational.


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## Voltage Regulation Loop

The output voltage is sensed and reduced to the reference level by the resistive divider consisting of R27, R28 and R 29 . The output voltage of this divider is sensed by the non-inverting input of the error amplifier and compared to the internal 4.0 V reference.

Assuming that the unit in not in a power limit condition, the voltage error signal will dominate the loop and be fed through the OR'ing network to provide one of the inputs to the reference multiplier. The other reference multiplier input is the divided down rectified AC input signal.

The output of this multiplier is a haversine signal that is an accurate replica of the input AC signal. The current shaping network compares the average current from the current sense amplifier to the reference voltage and forces this current to follow the AC reference voltage. The current out of the current sense amplifier is filtered at a frequency that is less than the switching frequency, but greater than the rectified line frequency.

This current is fed into the output filter capacitor(s) that filter it to a DC level.

## Power Regulation Loop

The power multiplier generates the product of the input current (from the current sense amplifier) and the AC rectified input voltage, to generate a signal that represents the input power of the unit. This signal is filtered to a frequency of less than the line frequency, so that it's output is a DC level.

If the load is increased to a level that exceeds the maximum power limit of the circuit, the output of the power multiplier will reach 2.5 V and the output of the power error amplifier will go to some level above ground. This signal will then override the signal from the voltage error amplifier (labeled "error amp" on the schematic), and will dominate the OR'ing network.
This signal then determines the level of the reference signal out of the reference multiplier, and determines the input current to the power converter. It should be noted that as this is a boost converter, the power limit circuit will only fold back the output voltage until it reaches the level of the peak line voltage. At this point the converter will shut down, but the input voltage will continue to charge the output capacitors through the rectifier.

## Shutdown Circuit

The shutdown circuit will inhibit the operation of the power converter and put the NCP1650 into a low power shutdown mode. To activate this circuit, apply 5.0 V to the red test point, with the black jack being "ground". Be aware that the black jack is actually hot as it is connected to the output of the input bridge rectifiers. An isolated 5.0 V supply should be used.
If this circuit is not being used, the terminals can be left open, as there is enough resistance built in to the circuit to keep the transistor (Q2) in it's off state.

PCB
The printed circuit board Gerber files are located on the ON Semiconductor website under the name NCP650- PCB1.


Table 1.

| Ref Des | Description | Part Number | Manufacturer |
| :---: | :---: | :---: | :---: |
| C2 | Cap, Ceramic, Chip, $0.1 \mu \mathrm{~F}, 50 \mathrm{~V}$ | C1608X7R1H104KT | TDK |
| C3 | Cap, Ceramic, Chip, . $012 \mu \mathrm{~F}, 50 \mathrm{~V}$ | C1608X7R1H123KT | TDK |
| C4 | Cap, Ceramic, Chip, $1.0 \mathrm{nF}, 50 \mathrm{~V}$ | C1608X7R1H102K | TDK |
| C5 | Cap, Ceramic, Chip, $0.022 \mu \mathrm{~F}, 50 \mathrm{~V}$ | C1608X7R1H223K | TDK |
| C7 | Cap, Ceramic, Chip, $22 \mu$ F, 6.3 V | C3225X5R0J226MT | TDK |
| C8 | Cap, Ceramic, Chip, $10 \mu \mathrm{~F}, 10 \mathrm{~V}$ | C3225X5R1A106MT | TDK |
| C9 | Cap, Ceramic, Chip, $4.7 \mu \mathrm{~F}, 10 \mathrm{~V}$ | C3216X5R1A475KT | TDK |
| C11 | Cap, Ceramic, Chip, 470 pF, 50 V | C1608C0G1H471JT | TDK |
| C14 | Cap, Ceramic, Chip, 470 pF, 50 V | C1608C0G1H471JT | TDK |
| C20 | $0.47 \mu \mathrm{~F}, 275 \mathrm{Vac}, \mathrm{X}$ Cap | ECQ-U2A474ML | Panasonic |
| C21 | Cap, Polyprop, $0.1 \mu \mathrm{~F}, 400 \mathrm{Vdc}$ | MKP1841-410-405 | Vishay-Sprague |
| C22 | Cap, Ceramic, Chip, $0.1 \mu \mathrm{~F}, 50 \mathrm{~V}$ | C1608X7R1H104KT | TDK |
| C23 | $100 \mu$ F, Alum Elect, 25 V | ECA-1EM101I | Panasonic |
| C25 | $100 \mu \mathrm{~F}$, Alum Elect, 450 V | ECO-S2WP100EX | Panasonic |
| C26 | Cap, Ceramic, Chip, $1.0 \mu \mathrm{~F}, 25 \mathrm{~V}$ | C3216X7R1E105KT | TDK |
| D1-D4 | Diode, Rectifier, $600 \mathrm{~V}, 3.0 \mathrm{~A}$ | 1N5406 | ON Semiconductor |
| D5 | Diode, Zener, 18 V , Axial Lead | MMSZ5248BT1 | ON Semiconductor |
| D6 | Diode, Signal, 75 V, 200 mA , SOT-23 | BAS19LT1 | ON Semiconductor |
| D7 | Diode, Ultra-Fast, $600 \mathrm{~V}, 8.0 \mathrm{~A}$ | MURHF860CT | ON Semiconductor |
| F1 | Fuse, 2.0 A, 250 Vac | 1025TD2A | Bussman |
| L1 | Inductor, $1000 \mu \mathrm{H}, 2.4 \mathrm{~A} \mathrm{Max}$ | CTX22-15557 | Coiltronics |
| L2 | 2.5 A Sat, $100 \mu \mathrm{H}$ Inductor, Diff Mode | TSL1315S-101K2R5 | TDK |
| L3 | 2.5 A Sat, $100 \mu \mathrm{H}$ Inductor, Diff Mode | TSL1315S-101K2R5 | TDK |
| Q1 | FET, 10.5 A, $0.7 \Omega, 600 \mathrm{~V}$, N-chl | FQP12N60 | Fairchild |
| Q2 | Bipolar Transistor, 50 V | MMBT2222ALT1 | ON Semiconductor |
| Q3 | FET, 1.0 A, 600 V , N-chl | FQP1N60 | Fairchild |
| R3 | Resistor, SMT, $810 \Omega$ | CRCW1206810JNTA | Vishay |
| R4 | Resistor, Axial Lead, $178 \mathrm{k}, \ldots$ Watt, 1\% | CMF-55-178K00FKRE | Vishay |
| R5 | Resistor, Axial Lead, $3.57 \mathrm{k}, \ldots$ Watt, $1 \%$ | CMF-55-3K5700FKBF | Vishay |
| R6 | Resistor, Axial Lead, $178 \mathrm{k}, \ldots$ Watt, 1\% | CMF-55-178K00FKRE | Vishay |
| R7 | Resistor, SMT, 8.6 k | CRCW12068K60JNTA | Vishay |
| R8 | Resistor, SMT, 9.1 k | CRCW12069K10JNTA | Vishay |
| R9 | Resistor, SMT, $56.2 \mathrm{k}, 1 \%$ | CRCW120656K2FKTA | Vishay |
| R10 | Resistor, SMT, 8.25 k, 1\% | CRCW12068K2FKTA | Vishay |
| R13 | Resistor, SMT, 51 k | CRCW120651K0JNTA | Vishay |
| R16 | Resistor, SMT, 10 | CRCW1206100JRE4 | Vishay |
| R20 | Resistor, Axial Lead, 10 k , _ Watt | CCF-07-103J | Vishay |
| R21 | Resistor, Axial Lead, 10 k , _ Watt | CCF-07-103J | Vishay |
| R22 | Resistor, Axial Lead, 10 k , _ Watt | CCF-07-103J | Vishay |
| R23 | Resistor, Axial Lead, 1.2 M, _ Watt | CCF-07-125J | Vishay |
| R25 | Resistor, SMT, 4.7 k | CRCW12064K70JNTA | Vishay |

Table 1. (continued)

| Ref Des | Description | Part Number | Manufacturer |
| :---: | :--- | :---: | :---: |
| R26 | Resistor, SMT, 12 k | CRCW120612K0JNTA | Vishay |
| R27 | Resistor, Axial Lead, 453 k,_ Watt, $1 \%$ | CMF-55-453K00FKBF | Vishay |
| R28 | Resistor, Axial Lead, 453 k,_ Watt, $1 \%$ | CMF-55-4533F | Vishay |
| R29 | Resistor, Axial Lead, $9.09 \mathrm{k}, \_$Watt, $1 \%$ | CCF-55-9K09FHR362 | Vishay |
| R30 | $1.0 \mathrm{~W}, 0.07 \Omega, 1 \%$ Resistor | WSL2512R0700FTB | Vishay |
| U1 | PFC Controller | NCP1650 | ON Semiconductor |
|  | Hardware |  |  |
| H1 | Printed Circuit Board | NCP1650-PWB1 | www.onsemi.com |
| H2 | Connector | 171602 | Weidmuller |
| H3 | Connector | 171602 | Weidmuller |
| H4 | Test Point, Red | 5005 | Keystone |
| H5 | Test Point, Black | 5006 | Keystone |
| H6 | Standoff, 4-40, Alum, Hex, .500 Inches | 8403 | HH Smith |
| H7 | Standoff, 4-40, Alum, Hex, .500 Inches | 8403 | HH Smith |
| H8 | Standoff, 4-40, Alum, Hex, .500 Inches | 8403 | HH Smith |
| H9 | Standoff, 4-40, Alum, Hex, .500 Inches | 8403 | HH Smith |
| H10 | Heatsink, TO-220 | $590302 B 03600$ | Aavid Thermalloy |
| H11 | Heatsink, TO-220 | $590302 B 03600$ | Aavid Thermalloy |

## Performance Data

Table 3. Regulation

| Line/Load | No Load | 50 Watts | 100 Watts |
| :---: | :---: | :---: | :---: |
| $85 \mathrm{~V}_{\text {rms }}$ | 405.5 | 405.1 | 403.9 |
| $115 \mathrm{~V}_{\text {rms }}$ | 405.6 | 405.2 | 404.3 |
| $220 \mathrm{~V}_{\text {rms }}$ | 405.4 | 405.5 | 404.9 |
| $265 \mathrm{~V}_{\text {rms }}$ | 438.4 | 405.5 | 405 |

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Table 4. Harmonics and Distortion

|  | 115 Vac, 100 Watts |  | 230 Vac, 100 Watts |  |
| :--- | :---: | :---: | :---: | :---: |
|  | V harmon | A harm. \% | V harmon | A harm. \% |
| $2^{\text {th }}$ | 0.084 | 0.03 | 0.169 | 0.12 |
| $3^{\text {rd }}$ | 0.505 | 2.8 | 0.722 | 2.6 |
| $5^{\text {th }}$ | 0.482 | 1.3 | 0.132 | 4.4 |
| $7^{\text {th }}$ | 0.168 | 0.5 | 0.075 | 0.17 |
| $9^{\text {th }}$ | 0.074 | 0.17 | 0.133 | 0.23 |
| $11^{\text {th }}$ | 0.088 | 0.13 | 0.134 | 0.17 |
| $13^{\text {th }}$ | 0.212 | 0.27 | 0.073 | 0.15 |
| $15^{\text {th }}$ | 0.324 | 0.37 | 0.265 | 0.28 |
| $17^{\text {th }}$ | 0.413 | 0.35 | 0.488 | 0.32 |
| $19^{\text {th }}$ | 0.632 | 0.31 | 1.12 | 0.44 |
| $P^{2}$ | - | 0.998 | - | 0.9928 |
| $T^{\text {HD }}$ (A) | - | 3.68 | - | 6.2 |
| $\mathrm{I}_{\text {fund }}$ | - | 0.919 | - | 0.451 |

Table 5. Efficiency

|  | $\mathbf{8 5} \mathrm{V}_{\text {rms }}$ | $\mathbf{1 1 5} \mathrm{V}_{\text {rms }}$ | $\mathbf{2 3 0} \mathrm{V}_{\text {rms }}$ | $\mathbf{2 6 5} \mathrm{V}_{\text {rms }}$ |
| :--- | :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\text {in }} @$ No Load | 2.87 | 4.06 | 5.07 | 5.11 |
| Pin | 108.8 | 106.9 | 103.2 | 103.7 |
| Vo | 403.2 | 404.3 | 404.9 | 405 |
| Io | 0.246 | 0.246 | 0.243 | 0.244 |
| Efficiency | 0.912 | 0.930 | 0.953 | 0.953 |

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